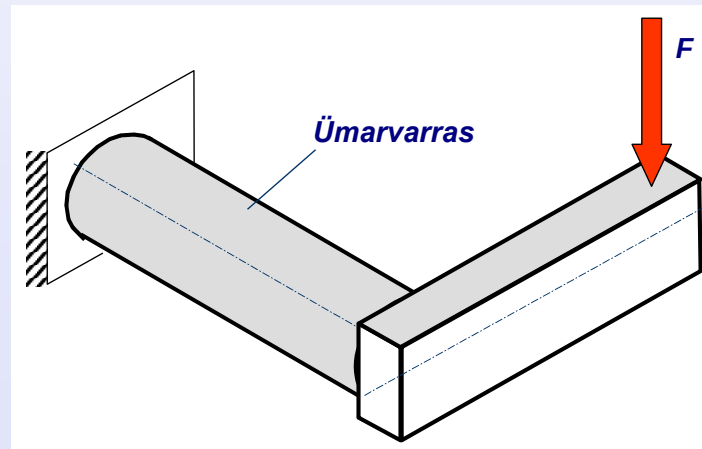


TUGEVUSÕPETUS

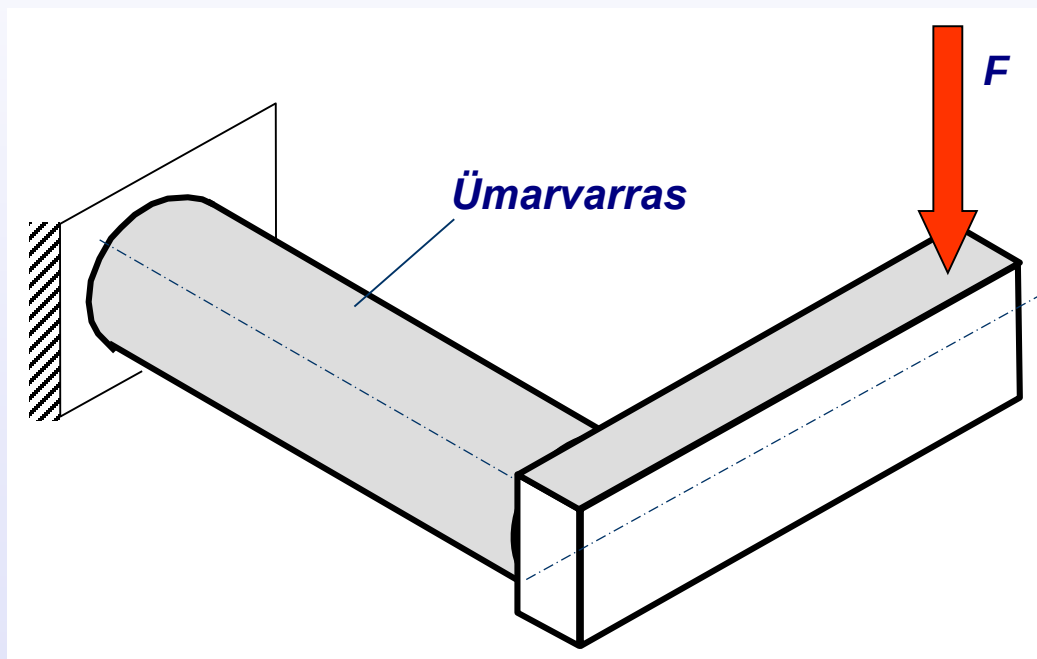
VÄÄNE + PAINE: Varda tugevuskontroll



1. Ülesande püstitus ja algandmed

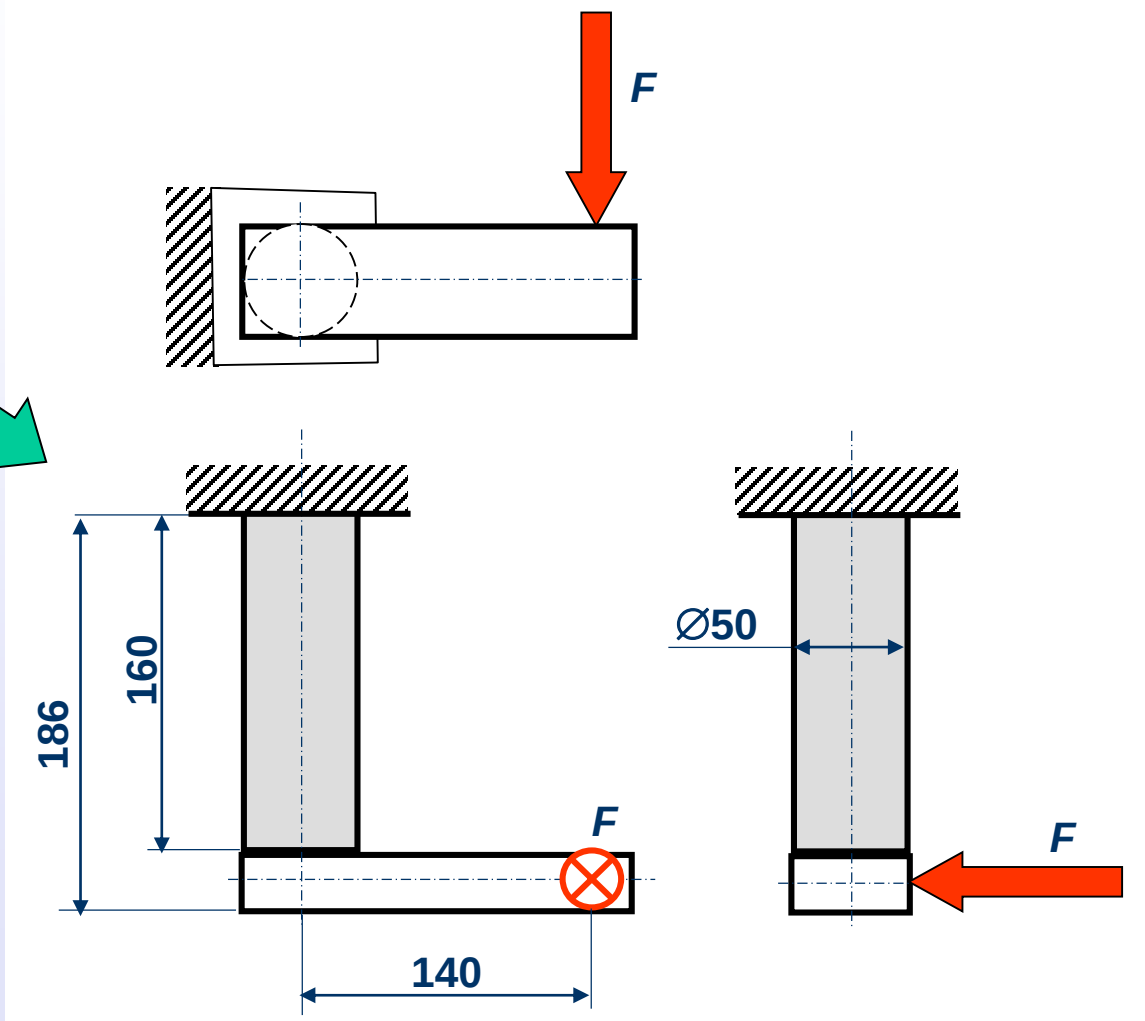
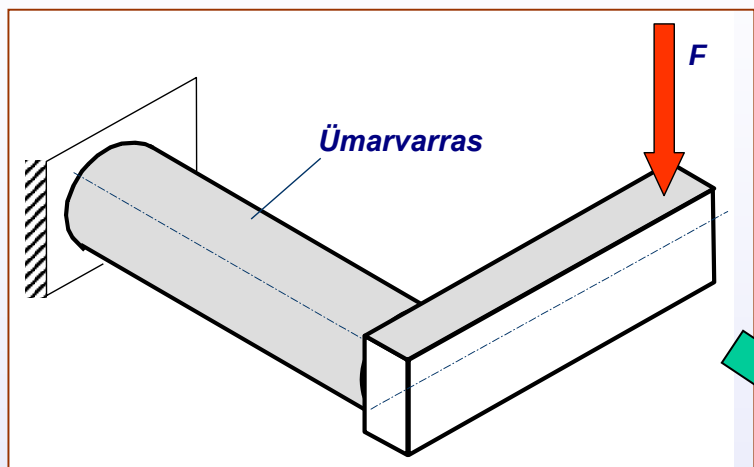
Kahe vardaga tarind

Kontrollida ümarvarda tugevust!



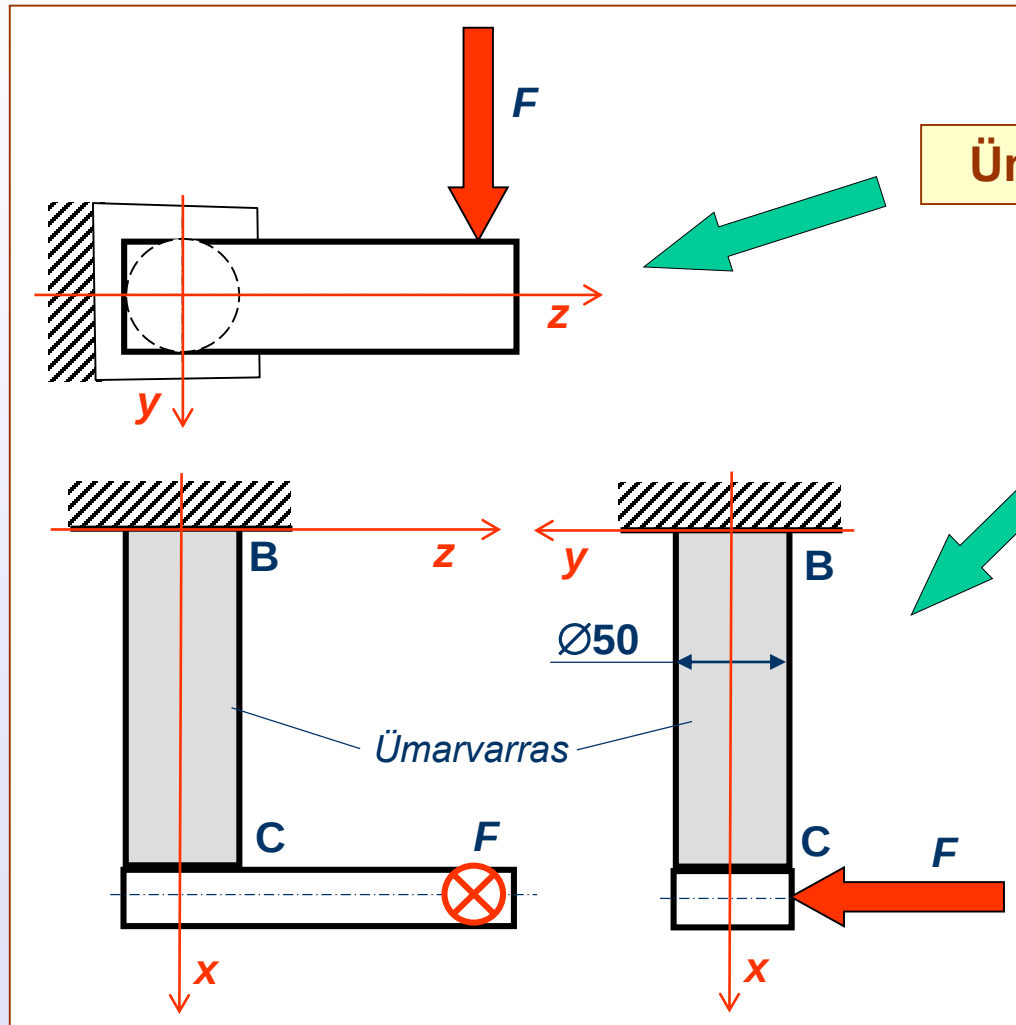
Tarindi koormus: $F = 10 \text{ kN}$
Ümarvarda läbimõõt: $\varnothing 50$
Ümarvarda materjal: teras S355
Ümarvarda nõutav varutegur: $[S] = 3$

Tarindi kolmvaade



2. Ümarvarda sisejõudude analüüs

2.1. Ümarvarda tööseisund



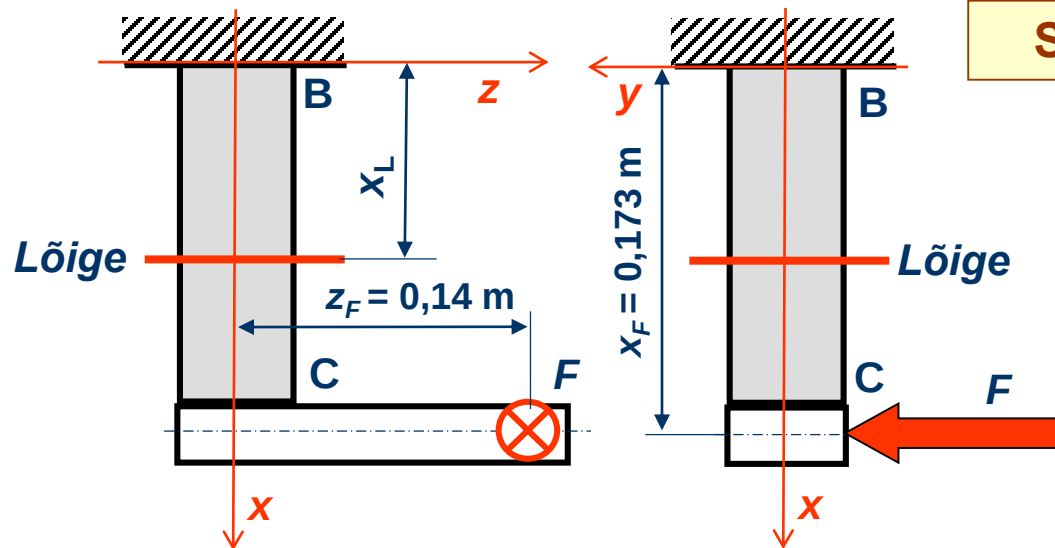
Ümarvarras on väänatud ümber telje x

Ümarvarras on painutatud tasandis xy ehk ümber telje z

Ümarvarras on koormuse F toimet tasandiliselt painutatud

Ümarvarda tööseisund on painde ja väände koosmõju

2.2. Ümarvarda sisejõud



Sisejõud arvutatakse lõikemeetodiga

Pöördemomentide
tasakaalutingimus telje x suhtes

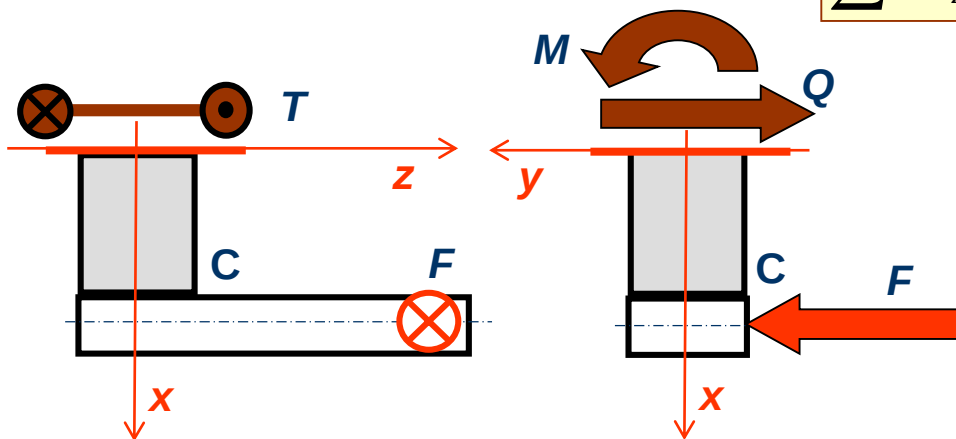
$$\sum \mathcal{M}_x = 0 \Rightarrow T - Fz_F = 0$$

$$T = T_B = T_C = Fz_F = 10^4 \cdot 0,14 = \underline{1400 \text{ Nm}}$$

Pöördemomentide
tasakaalutingimus telje z suhtes

$$\sum \mathcal{M}_z = 0 \Rightarrow M - F(x_F - x_L) = 0 \quad M = F(x_F - x_L)$$

Lõige



Kui $x_L = 0$, siis:

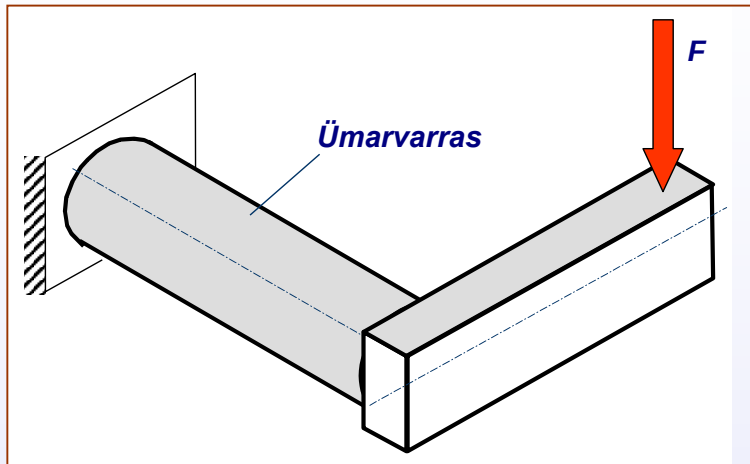
$$M = M_B = 10^4 \cdot (0,173 - 0) = \underline{1730 \text{ Nm}}$$

Kui $x_L = BC = 0,16 \text{ m}$, siis:

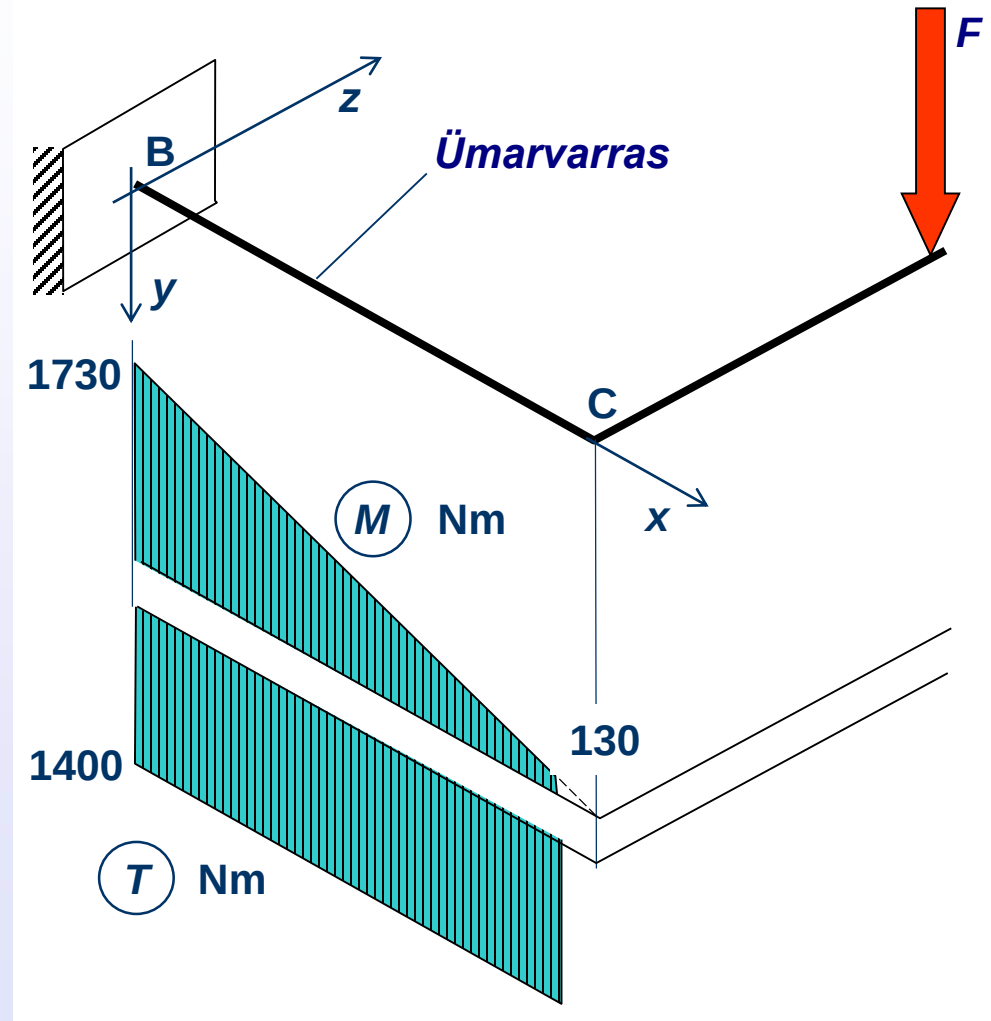
$$M = M_C = 10^4 \cdot (0,173 - 0,16) = \underline{130 \text{ Nm}}$$

Põikjõu Q arvestamisest loobutakse

2.3. Ümarvarda sisejõudude epüürid



Ühtlase ÜMARvõlli ohtlik
ristlõige on B



2.4. Ümarvarda ekvivalentne paindemoment

Ekvivalentne paindemoment

$$M_{\text{Ekv}}^{\text{III}} = \sqrt{M_y^2 + M_z^2 + T^2} = \sqrt{M^2 + T^2}$$

Varda ekvivalentsed paindemomendid

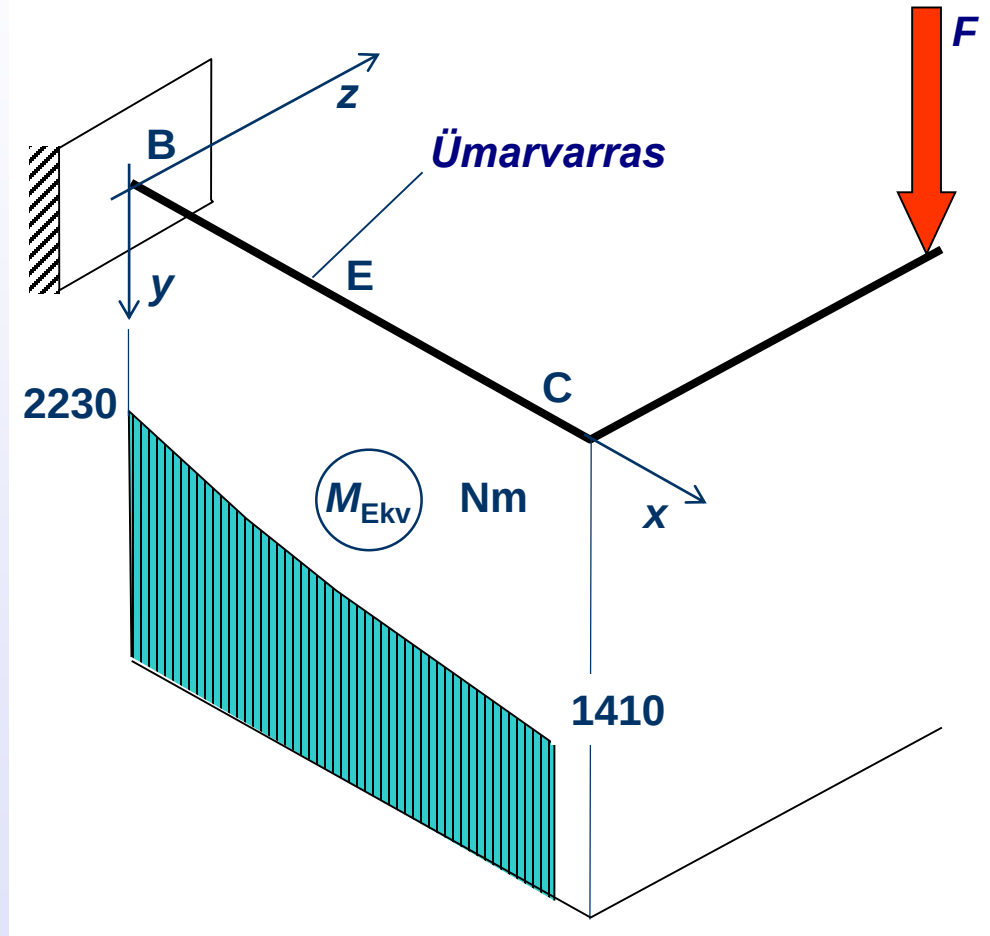
$$\begin{aligned} M_{\text{Ekv}, B}^{\text{III}} &= \sqrt{M_B^2 + T_B^2} = \\ &= \sqrt{1730^2 + 1400^2} = 2225,8 \approx \underline{2230 \text{ Nm}} \end{aligned}$$

$$\begin{aligned} M_{\text{Ekv}, C}^{\text{III}} &= \sqrt{M_C^2 + T_C^2} = \\ &= \sqrt{130^2 + 1400^2} = 1406 \approx \underline{1410 \text{ Nm}} \end{aligned}$$

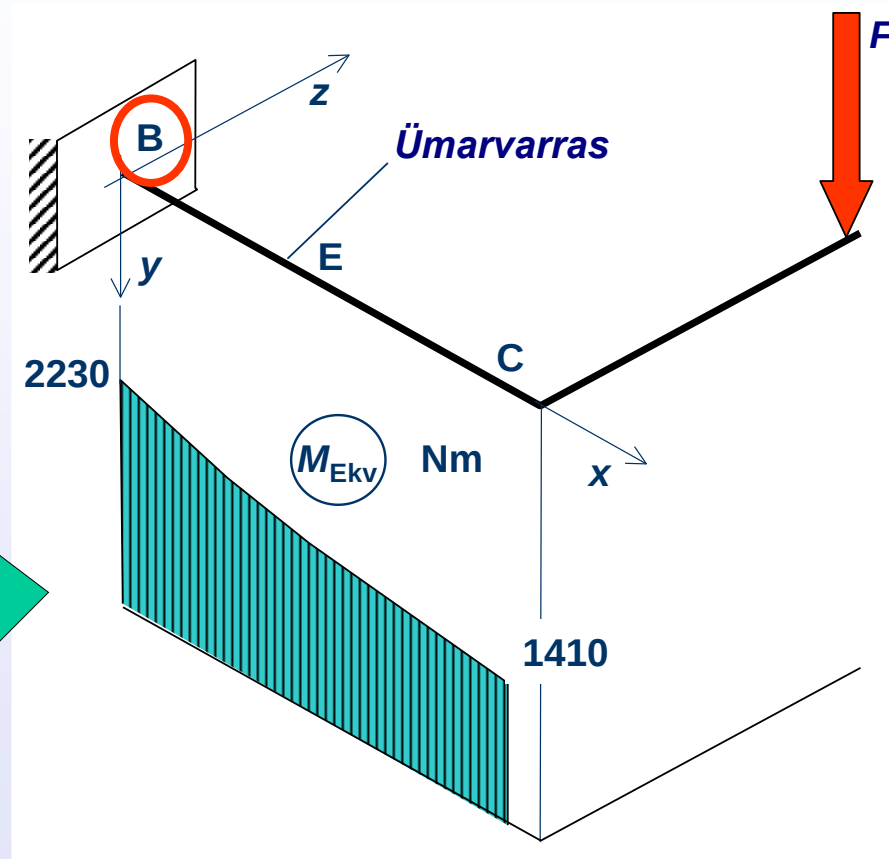
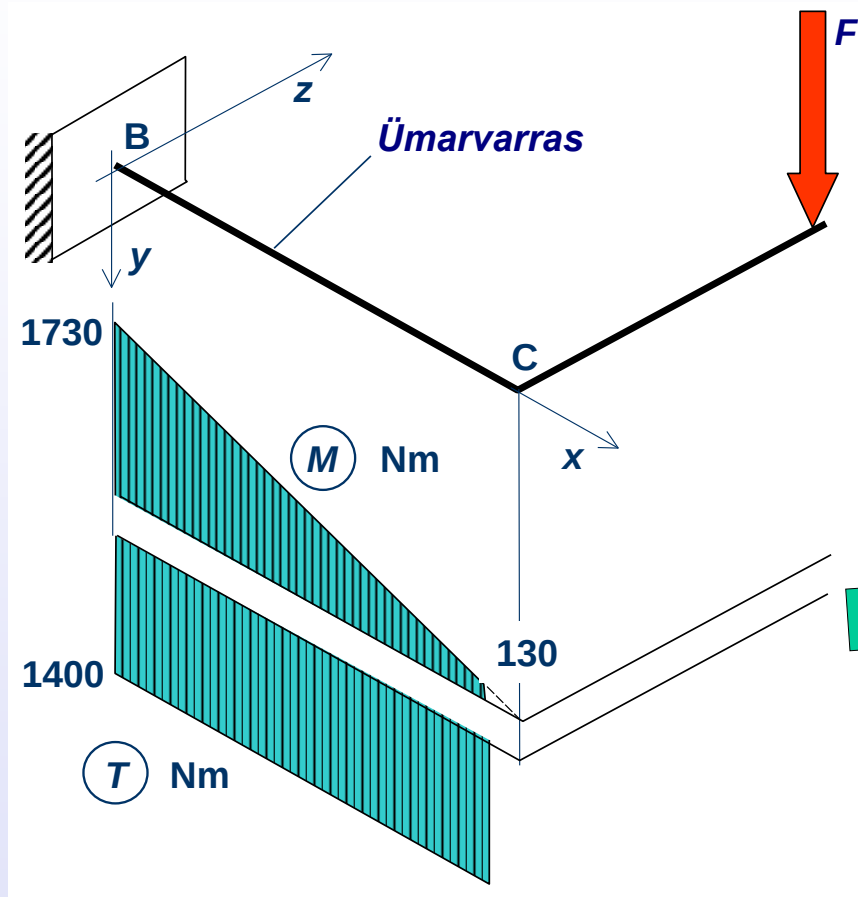
$$\begin{aligned} M_{\text{Ekv}, E}^{\text{III}} &= \sqrt{M_E^2 + T_E^2} = \\ &= \sqrt{930^2 + 1400^2} = 1680 \text{ Nm} \end{aligned}$$

$BE = EC \rightarrow M_E = 930 \text{ Nm}$

Abipunkt epüüri joonestamiseks



2.5. Ümarvardasisejüudude analüüs



Ühtlase ÜMARvõlli ohtlik ristlõige on B

$$M_{\text{Ekv}, B}^{\text{III}} = 2230 \text{ Nm}$$

3. Ümarvarda tugevusarvutus

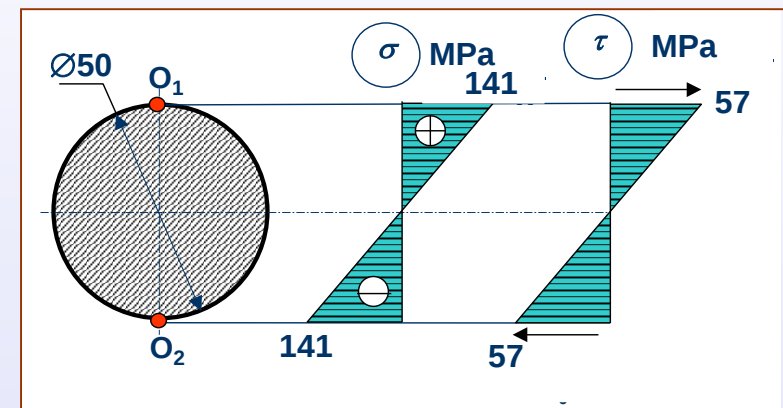
3.1. Ümarvarda suurimad pinged

Suurim paindepinge ümarvarda ohtlikus lõikes B

$$\begin{aligned}\sigma_{\max} &= \frac{M}{W} = \frac{32M}{\pi D^3} = \\ &= \frac{32 \cdot 1730}{\pi \cdot 0,05^3} = 140,9 \cdot 10^6 \text{ Pa} \approx \underline{141 \text{ MPa}}\end{aligned}$$

Suurim väändepinge ümarvarda ohtlikus lõikes B

$$\begin{aligned}\sigma_{\max} &= \frac{T}{W_0} = \frac{16T}{\pi D^3} = \\ &= \frac{16 \cdot 1400}{\pi \cdot 0,05^3} = 57,04 \cdot 10^6 \text{ Pa} \approx 57,0 \text{ MPa}\end{aligned}$$



3.2. Ümarvarda tugevusvarutegur

Võrdpinge ümarvarda ohtliku lõike B ohtlikes punktides

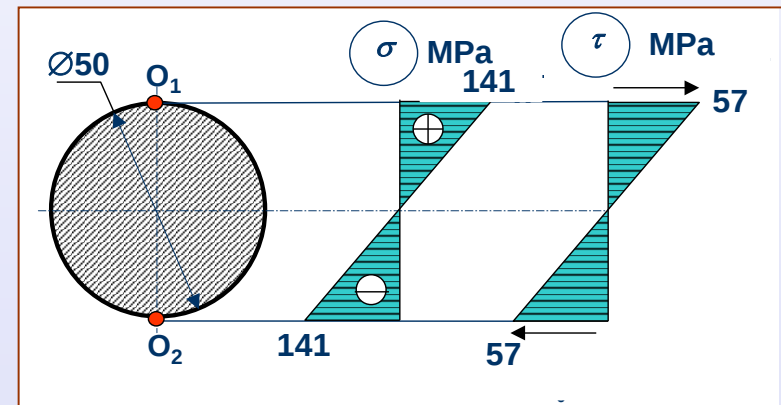
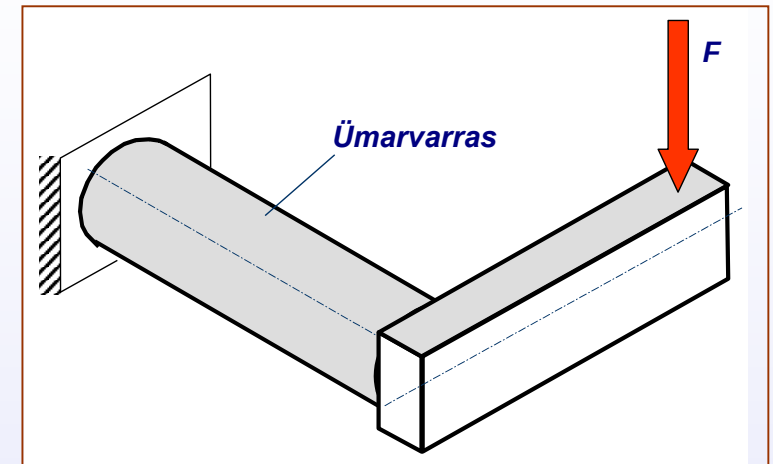
$$\begin{aligned}\sigma_{\text{Ekv}} &= \frac{M_{\text{Ekv}}}{W} = \frac{32M_{\text{Ekv}}}{\pi D^3} = \\ &= \frac{32 \cdot 2230}{\pi \cdot 0,05^3} = 181,7 \cdot 10^6 \text{ Pa} \approx \underline{182 \text{ MPa}}\end{aligned}$$

Ümarvarda vähim tugevusvarutegur

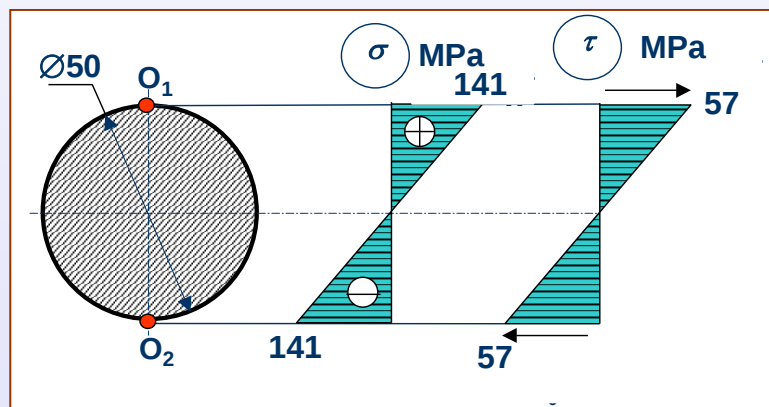
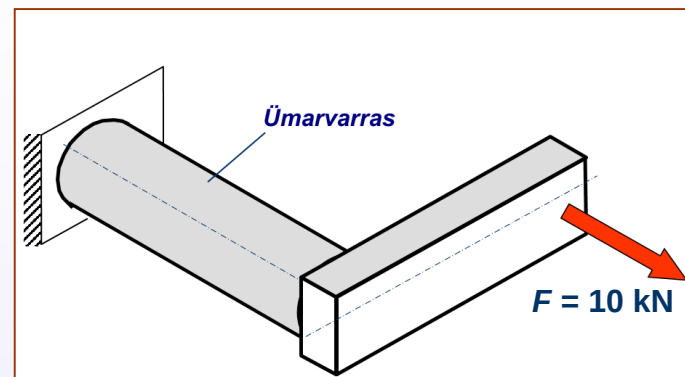
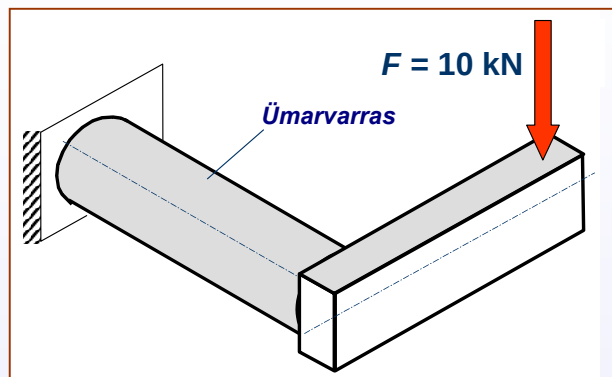
$$S = \frac{\sigma_y}{\sigma_{\text{Max}}} = \frac{355}{182} = 1,95 \approx 1,9 < \underline{[S] = 3}$$

Ümarvarda Ø50 tugevus EI OLE piisav

Konstruksiooni või koormusseisundit tuleb muuta või valida tugevam materjal

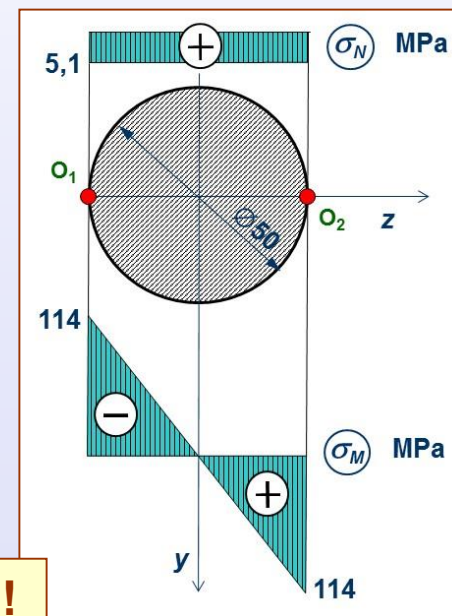


3.3. Tulemuste võrdlus



$$S = 1,9$$

$$S = 2,9$$



Tarindi tugevusvaru sõltub koormusskeemist!!!